SOTERIA FINAL WORKSHOP



DOSE-DEPENDENT NANO-FEATURES AND THEIR EFFECT ON INTER-GRANULAR CRACKING SUSCEPTIBILITY (INTERNALS)

<u>OUTLINE</u>

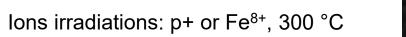
- Previous findings, up to PERFORM60 (up to 2012)
- Subsequent sub-grain modelling developments (2012-)
- Observations and poly-crystalline model (SOTERIA 2015-2019)

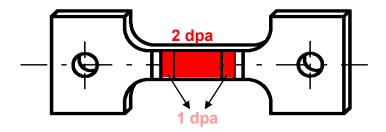
Contribution to SOTERIA WP2 Co-workers: B. Tanguy, J. Hure Speaker: **Christian Robertson**

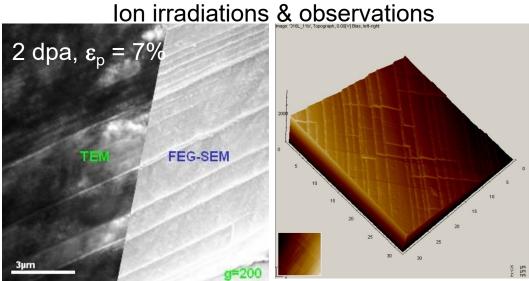


Post-irradiation plasticity mechanisms



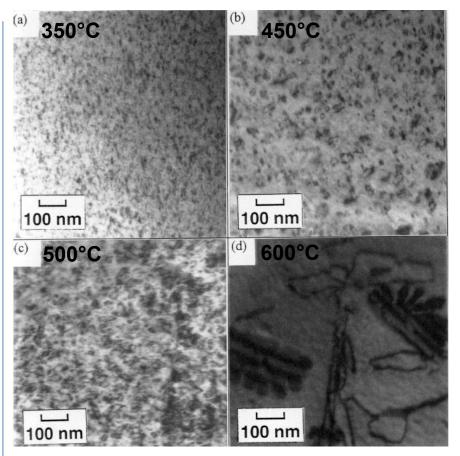




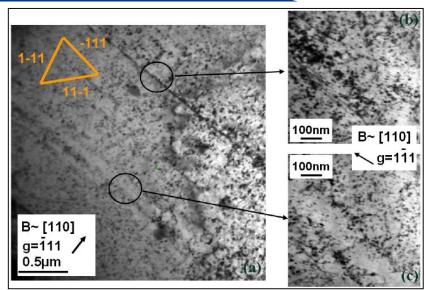


Irradiation defect microstructure





C.Robertson (1998), 3 dpa, Kr ions



Deformation: in the form of shear bands

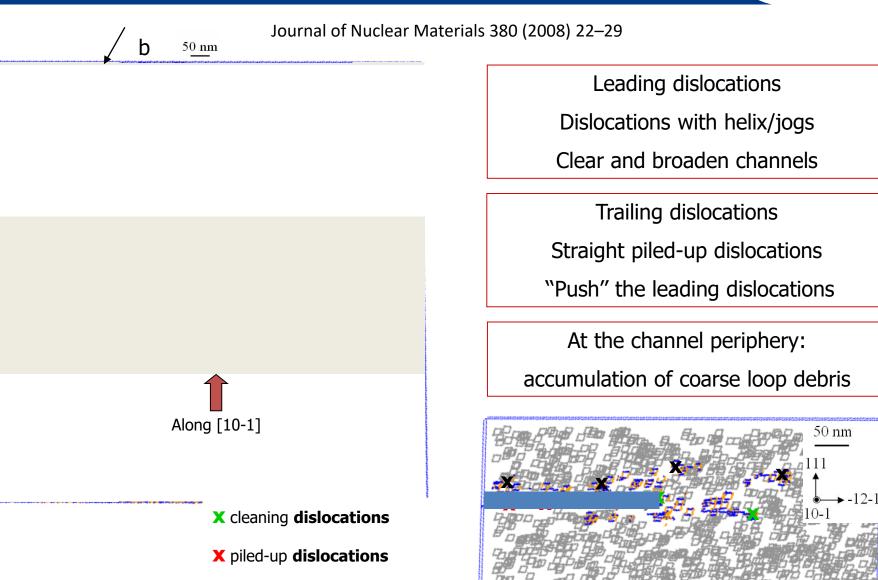
- i. Dislocation pile-ups: $L_{PU} \propto D_{q}$
- ii. Secondary shear bands and then gradual band broadening



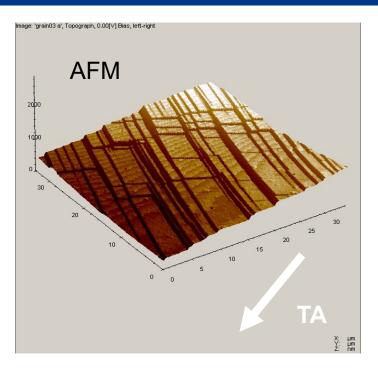
Shear band dislocation substructure

X arrested **dislocations**

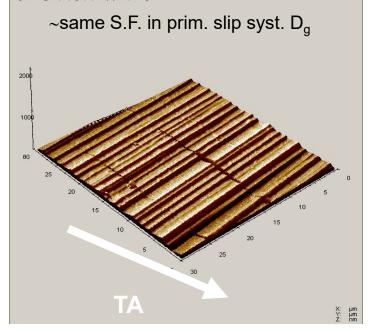


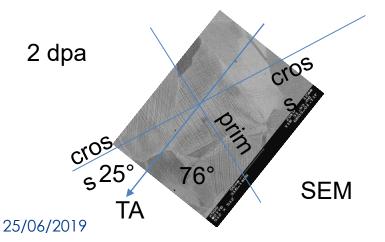


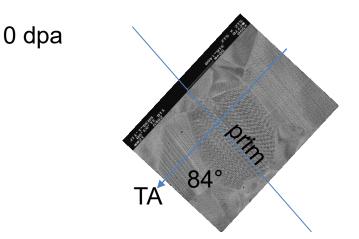
Post-irradiation plasticity mechanisms (P60)



age: '316L_45a', Topograph, 0.00[∨] Bias, left-right





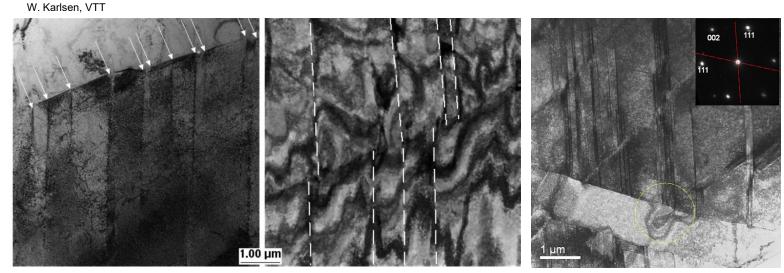


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Partial summary... (up to P60)



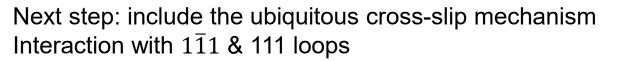
- Slip steps are fewer and smaller, after irradiation @ strain localization
- Loop-depleted channel (or clear band) is merely a particular shear-band type
- Channels include dislocation pile-ups (unlike in BCC, where tangles form), generating a long-range, out of plane stress field
- Channel (shear band) thickness and spacing controls the stress concentration magnitude at the GBs and hence, crack initiation susceptibility thereof



0.89 dpa 304L Tensile test B7, specimen "nec4"

11 dpa CW 316 Tensile test B7, specimen "nec4"

Cross-slip: interaction with defects



NUMODIS @ MD validated: Journal of Nuclear Materials 460 (2015) 37-43

Cross-slipped arm b = [111]Y[110] $(1\bar{1}0)$ X[112] (z[111] B(C)

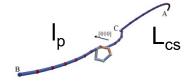
Y. Li, C. Robertson, Model. Simul. Mater. Sci. Eng. 26 (2018) 055009

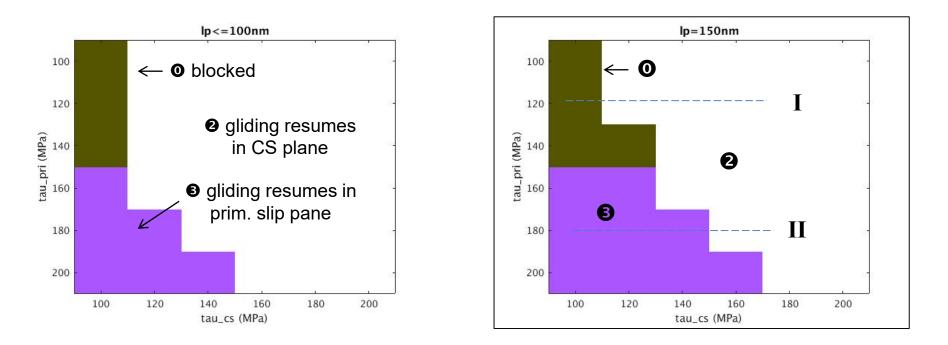


Cross-slip: interaction with defects



Stress controlled simulations I_p : segment length in primary SS $I_p + L_{cs} = 300 \text{ nm}$



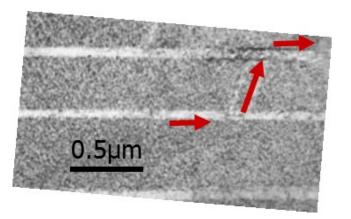


In presence of cross-slip: interaction strenght < loop strength
 Cross-slip provides an easy path to overcome the defects

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Cross-slip: shear band multiplication

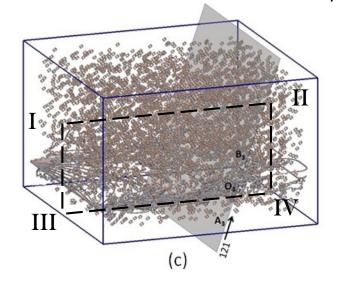




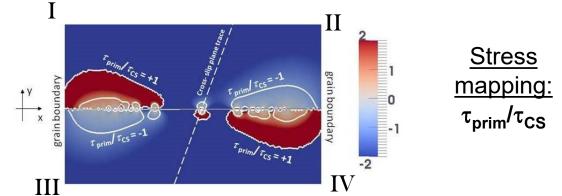
Regular inter-channel spacing \leftrightarrow secondary channel in X-slip planes: [Yao 2005]

Secondary channels develop wherever CS probability is high, i.e. wherever effective defect interaction strength is minimal (path of least interaction)

In presence of obtacles P(cross-slip) highest: $\tau_{prim}/\tau_{CS} = \pm 1$



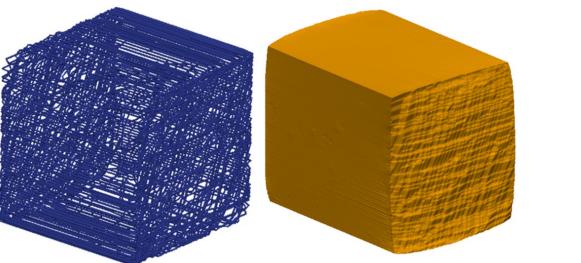
K. Gururaj etal, Phil. Mag. 95 No.12 (2015) 1368-1389

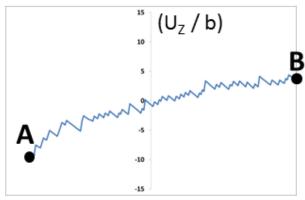


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Shear band spacing scales with internal stress field characteristic distance

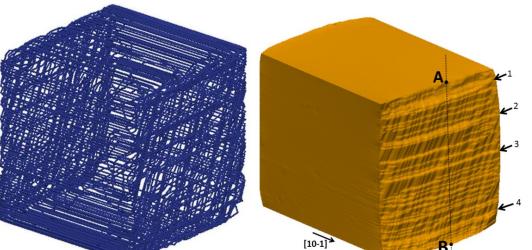
Shear band spacing: simulation...

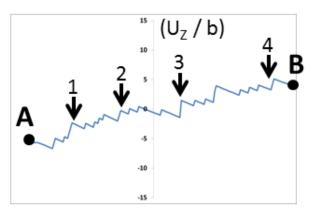




00 loops



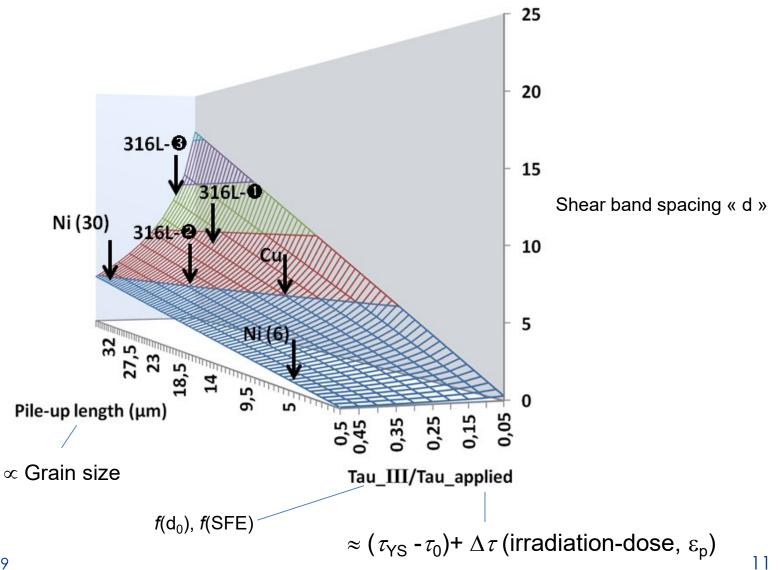




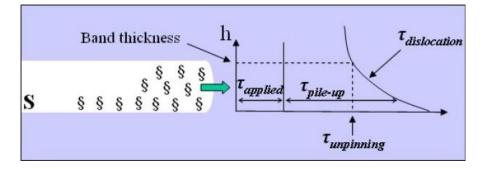
10²² loops/m³ (~ 0.5 dpa)

Shear band spacing prediction?



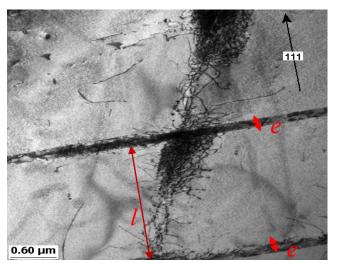


Shear band thickness prediction ?



Dislocation can glide inside shear bands wherever verifies:

 $\tau_{app} + \tau_{pu(band)} > \tau_{defect}$



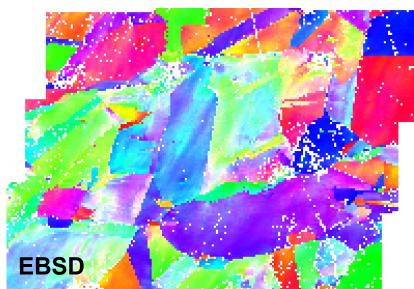
[W. Karlsen, VTT, 2006]

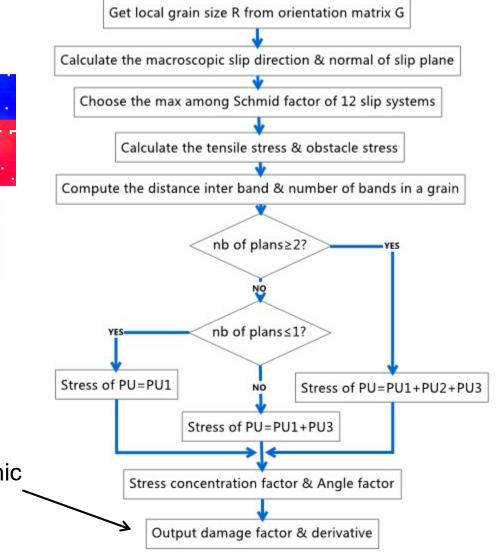
How to chose these different terms?

- \checkmark Applied stress level τ_{app} (tensile testing data or hardening theory)
- $\approx \tau_{pu}$ (inter-band long pile-ups, analytical H&L model)
- The obstacle strength τ_{defect} (MD & continuum S&B theory).
- $rac{app}{app} \& \tau_{obs}$ relate to the irradiation conditions
- Defect cluster size
- Defect cluster number density
- Other hardening mechanisms?

Application to poly-crystals



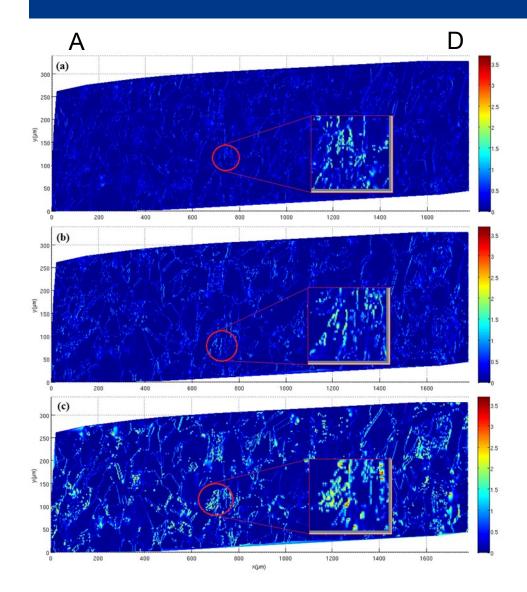




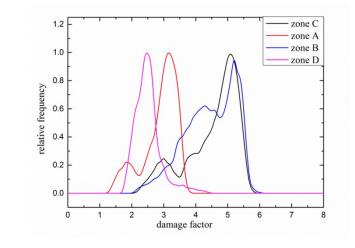
Damage factor include stress concentration and crystallographic orientation contributions.

Application to poly-crystals





Zone to zone variations of GB loading

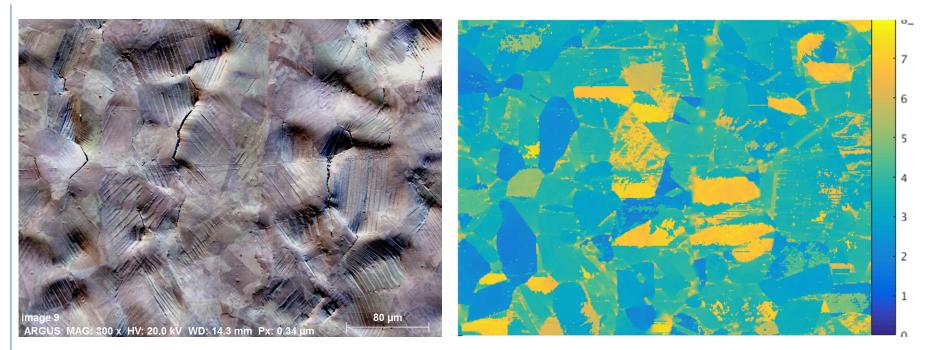


Effect of rising dose on GB loading



Comparison with observation (P+ irradiation)





[B. Tanguy, DEN/DMN/SEMI]

Irradiated 316L steel p+ 2dpa/350°C, 10⁻⁷ s⁻¹ up to $\epsilon_P = 4\%$ in autoclave (primary water) Applied stress considering the hardening effect: 684MPa, Area: 411.02 µm X 298.92µm Mean Defect cluster size: 13.8nm, defect number density 3.6e22 m⁻³



Comparison with observation (P+ irradiation)

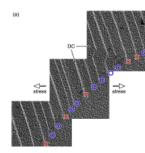


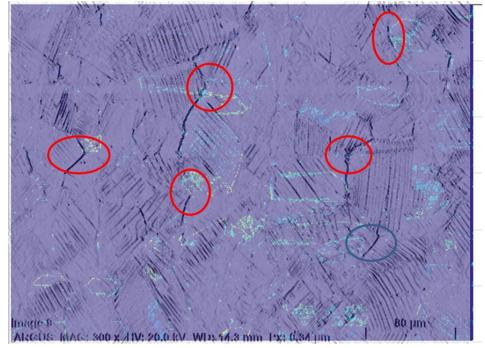


- Damage threshold identification (quantitative evaluation)
- Correct crack nucleation probability in surface grains

Most likely to crack nucleation sites: GB presenting the largest plastic strain contrast.

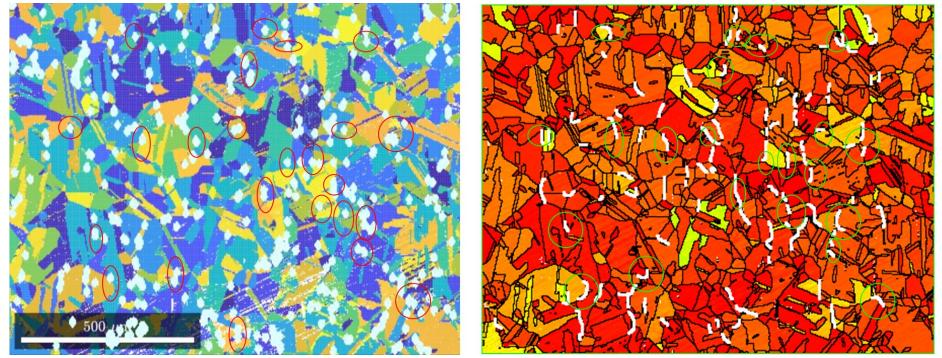
He, Johnson, Was, Robertson Acta Materialia 138 (2017) 61-71





Comparison with observation (Fe irradiation)



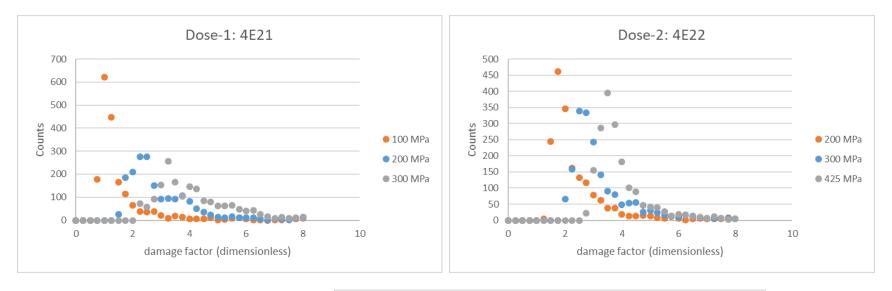


[B. Tanguy, DEN/DMN/SEMI]

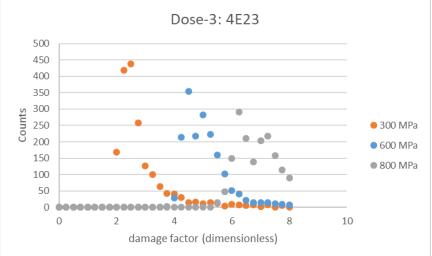
- Predicted crack length comparable to observed crack length
- Crack initiation site correspondance at least 50%
- Damage threshold(s) identification: (mostly) confirmed

Model predictions





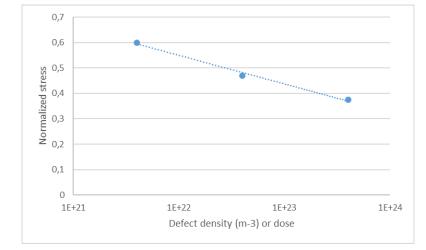
 Including a stress correction according to GB surface energy

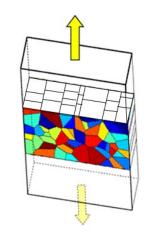


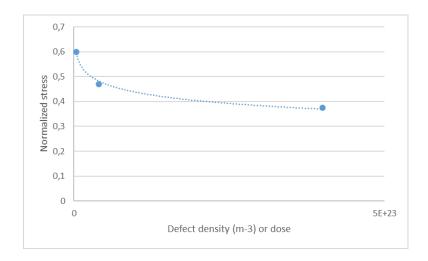
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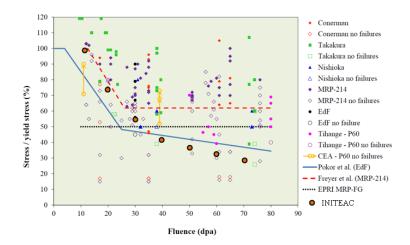
Model predictions













Conclusion & Perspectives



Analysis of plastic strain spreading in presence of disperse defect populations:

- Dislocation displacement is controlled by <u>cross-slip</u>: i-helps mobile dislocations **overcoming** the disperse defect clusters (enables choosing path of least interaction), ii-helps **spreading** shear bands across the whole grain (secondary channel formation)
- Shear bands dislocation substructures include extended dislocation pile-ups
- Shear band spacing controlled by grain-wide pile-ups
- Shear band broadening is gradual; controlled by inter-band wide pile-ups
- Grain boundary stress \rightarrow depend on shear bands distribution
- Inter-granular crack initiation susceptibility is higher wherever the **plastic strain contrast** is maximal, between adjacent pairs of grains

Perspectives:

- Improve the estimation of applied stress level, including additional hardening mechanisms (dislocation source decoration)
- Consider 3D effects of grain diameter versus grain depth
 25/06/2019

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Shear band multiplication: cross-slip

Cross-slip of a bowed-out screw, due to obstacles

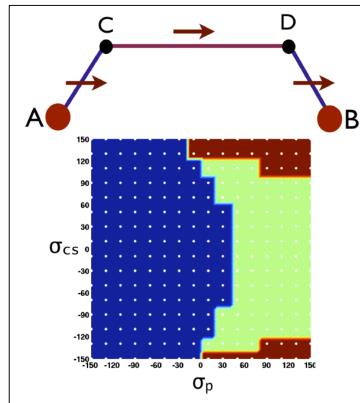


Figure 6.12 – The set-up and result corresponding to the set 9 of the table 6.3. The image on the left is explained in the text. The image on the right corresponds to the result of primary and cross-slip stress acting on this configuration. The x-axis refers to the stress acting on the primary slip system, $\sigma_p = \vec{\sigma} \cdot n_p$. In MPa and y-axis is the stress resolved in the cross-slip plane, $\sigma_{cs} = \vec{\sigma} \cdot n_{cs}$. In MPa The regions in red indicate the (σ_p, σ_{cs}) combination that makes the length CD equal to AB, and region in blue indicates the (σ_p, σ_{cs}) combination that makes the length CD tend to zero. The regions in green indicate the (σ_p, σ_{cs}) values where the length of cross-slip segment CD neither goes to 0 nor equals distance between pinning points AB.

- In presence of obstacles (radiation defects, GB, etc), cross-slip probability is maximal for τ_{prim}/τ_{CS} = ±1

- This validates our model for predicting interband distance in irradiated metals (see 06/13)

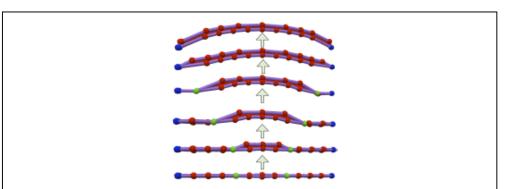
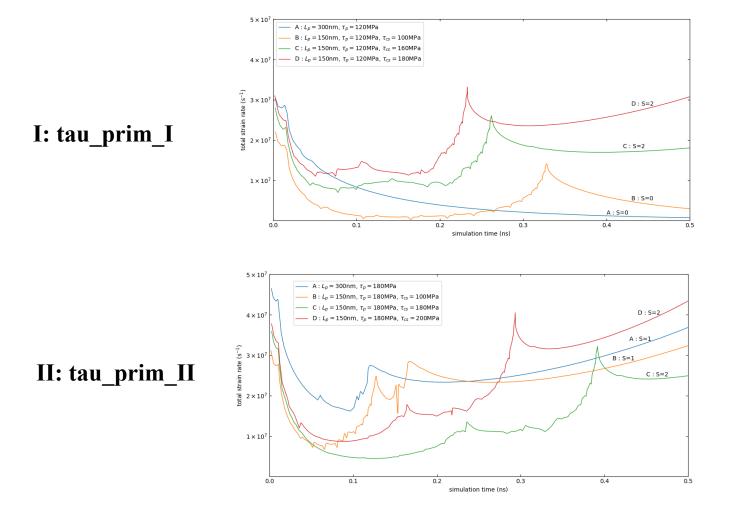


Figure 6.8 – The evolution of a three segment split composite FR source of the form shown in the figure 6.5b. The figures from top to bottom illustrate the cross-slip segment spreading over the whole dislocation length.

Cross-slip: interaction with defects



Rising tau_CS facilitates dislocation unpinning regarless of tau_prim!

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